

On Handling the Inverse Analysis of Passive Spectroscopic Cargo Monitoring Data

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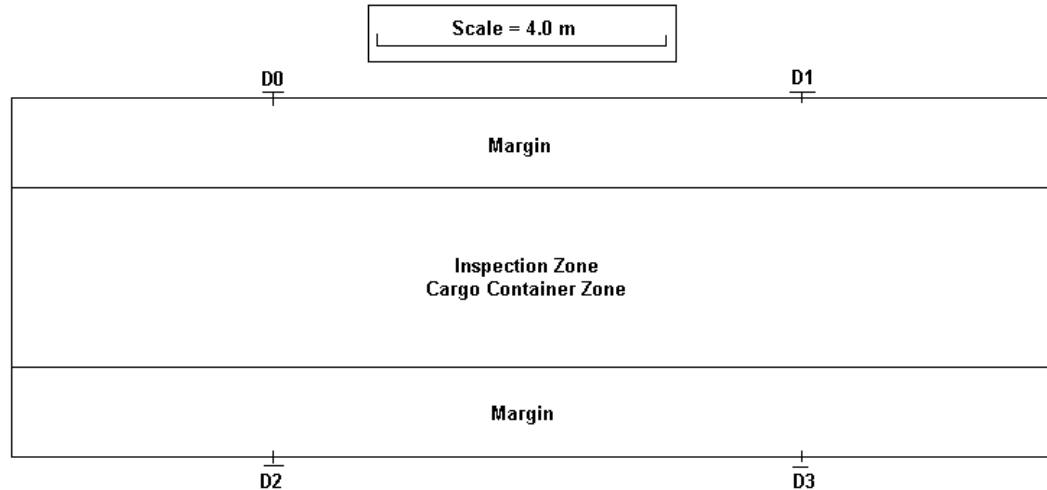
Introduction

- Passive gamma spec is costly as a cargo monitoring technology, and it has serious limitations.
- Possibly more useful when combined with other technologies like neutron counting
 - But then again, a neutron alarm alone should be enough to warrant more invasive action
- Cost-benefit analysis is controversial

Objectives

- Apply Monte Carlo Library Least Squares
- Use few to no high-resolution spectrometers
- Source strength ID
 - ‘radioisotope weigh station’
 - resistant to intentional shielding
- Source location
 - Security need
- Demonstrate new methodology

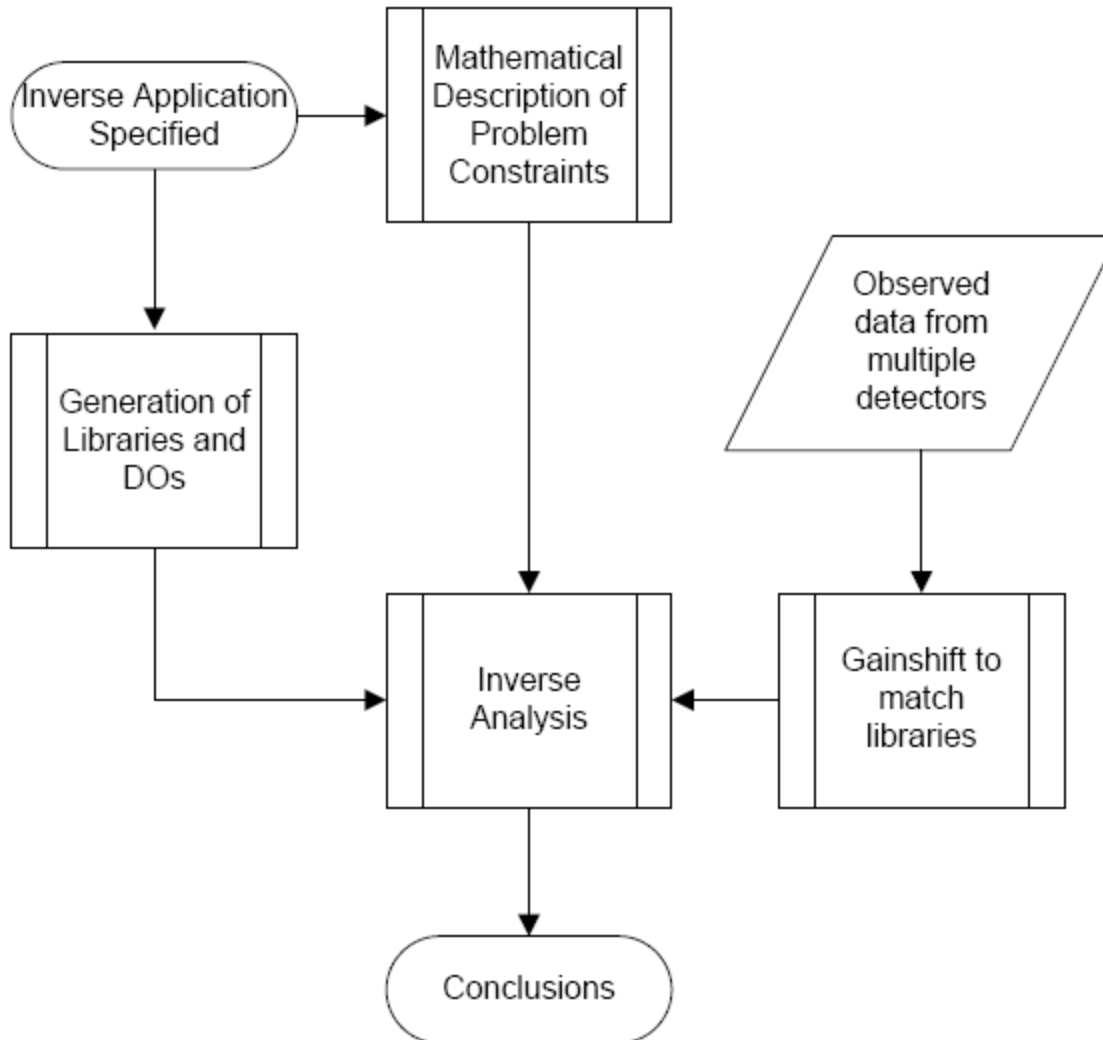
Example Schematic



2-D approximation of secondary screening of 48' semi-tractor trailer by quad-panel Advanced Spectroscopic Portal

Inter-comparison of MCLLS results for separate detectors at known positions yields most likely source position, activity, and shielding configurations.

Overview



Parameterize sources of variability to model detector response

Impose as much constraint as possible

Express parameterization in 3d transport simulation, estimating reference spectra and DOs

Process measurement data for comparison to simulation

Then, conduct lin/non-linear searches through parameter space and apply constraints as appropriate

Second degree expansion

- In three variables, types of shielding
- With a scalar multiplier

$$\begin{aligned} \vec{f}(\vec{x} + \Delta\vec{x}) = \alpha & \left[\vec{f}_1(\vec{x}_0) + \frac{\partial \vec{f}_1}{\partial x_1} \Delta x_1 + \frac{\partial \vec{f}_1}{\partial x_2} \Delta x_2 + \frac{\partial \vec{f}_1}{\partial x_3} \Delta x_3 + \frac{1}{2} \frac{\partial^2 \vec{f}_1}{\partial x_1^2} \Delta x_1^2 + \frac{1}{2} \frac{\partial^2 \vec{f}_1}{\partial x_2^2} \Delta x_2^2 + \frac{1}{2} \frac{\partial^2 \vec{f}_1}{\partial x_3^2} \Delta x_3^2 \right. \\ & + \left(\frac{\partial^2 \vec{f}_1}{\partial x_1 \partial x_2} + \frac{\partial^2 \vec{f}_1}{\partial x_2 \partial x_1} \right) \Delta x_1 \Delta x_2 + \left(\frac{\partial^2 \vec{f}_1}{\partial x_1 \partial x_3} + \frac{\partial^2 \vec{f}_1}{\partial x_3 \partial x_1} \right) \Delta x_1 \Delta x_3 \\ & \left. + \left(\frac{\partial^2 \vec{f}_1}{\partial x_2 \partial x_3} + \frac{\partial^2 \vec{f}_1}{\partial x_3 \partial x_2} \right) \Delta x_2 \Delta x_3 \right] \end{aligned}$$

- References and derivatives estimated by MC simulation

Unraveling Location and Intensity

$$\alpha = c \frac{I}{\varepsilon_{i,k}(\mu_{xx})}$$

- Intensity
- Efficiency
- Cross-section

Location and Intensity

- Given a histogram probability distribution for path lengths through a detector centered at an origin as a continuous function of isotropic source position one may...

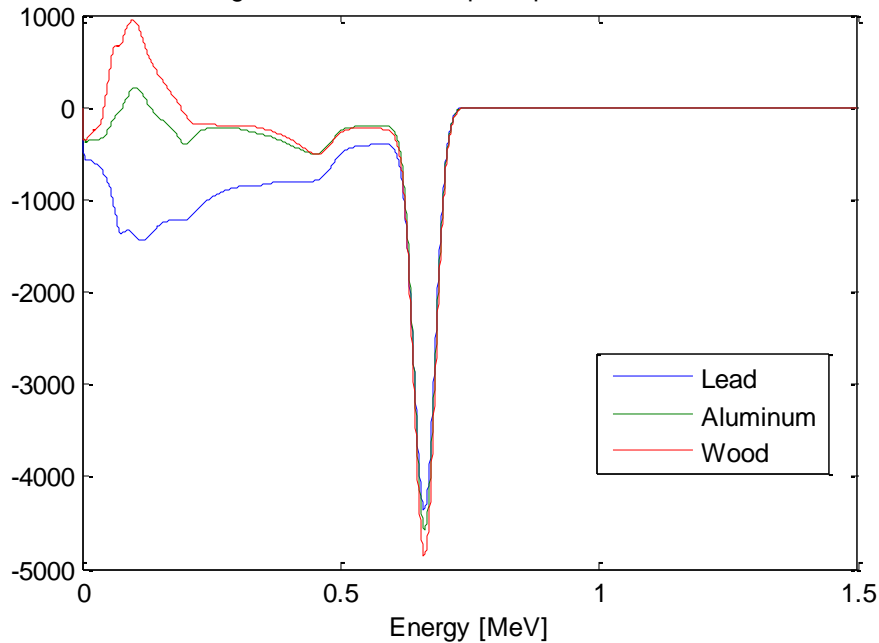
$$\bar{P}_{\ell_i} = \frac{\iiint_{V_i} dV_i P_{\ell}(x, y, z)}{\iiint_{V_i} dV_i}$$

$$\frac{1}{\varepsilon_{i,k}(\mu_x)} \cong \sum_m e^{-\bar{P}_{\ell_{i,m}} \ell_m \mu_x}$$

First Finite Differences

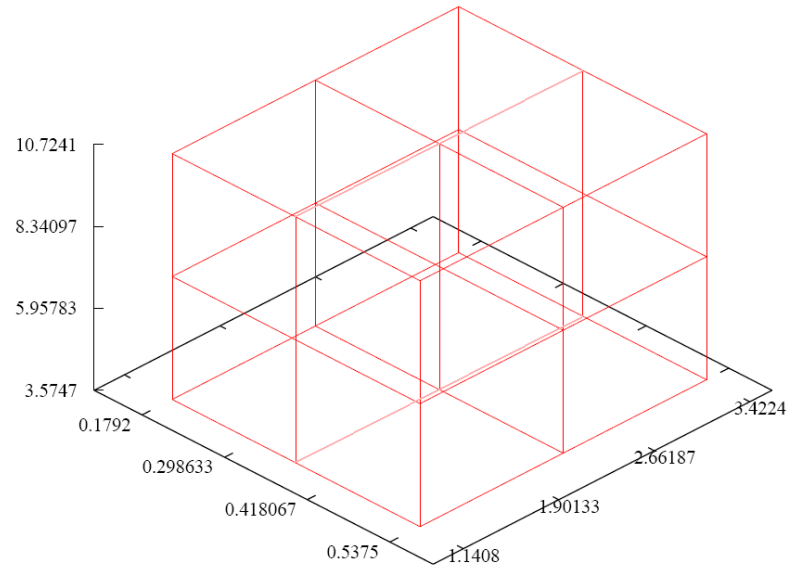
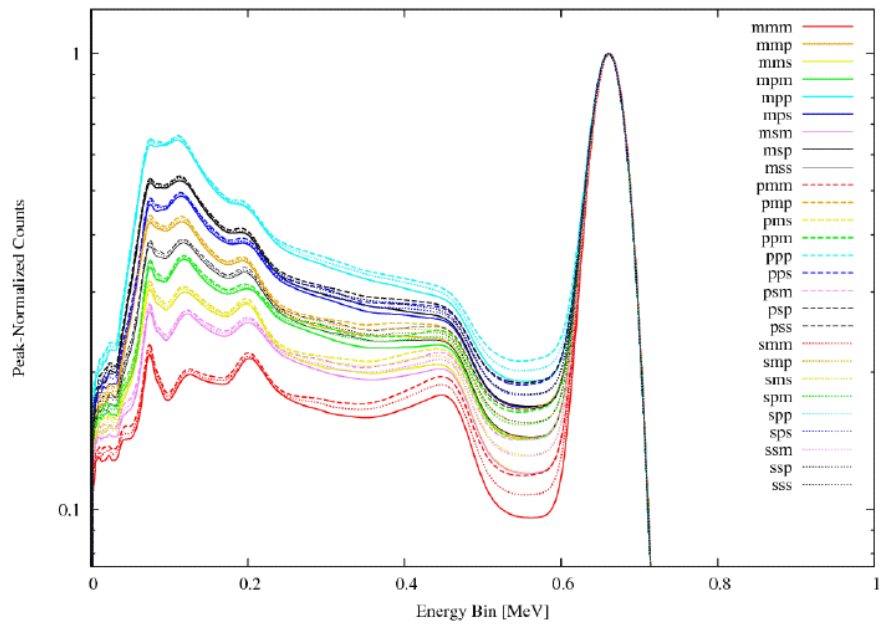
$$\frac{\partial \vec{f}_1}{\partial x_1} \approx \frac{\vec{f}_1(x_{1,p}, x_{2,s}, x_{3,s}) - \vec{f}_1(x_{1,m}, x_{2,s}, x_{3,s})}{2h_1}$$

First order shielding derivatives Counts per h per 20mCi Cs-137 at 1m, 2x4 NaI

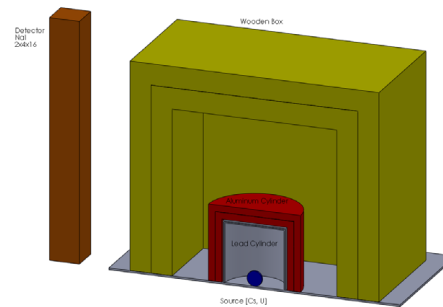


	Pb [cm]	Al [cm]	Wood [cm]
50%	0.53754	3.42235	10.72411
Standard	0.358364	2.281566	7.1493867
-50%	0.179182	1.140782	3.57470333

$$\vec{f}(\vec{x} + \Delta\vec{x}) = a \left[\vec{f}_1(\vec{x}_0) + \frac{\partial \vec{f}_1}{\partial x_1} \Delta x_1 + \frac{\partial \vec{f}_1}{\partial x_2} \Delta x_2 + \frac{\partial \vec{f}_1}{\partial x_3} \Delta x_3 \right]$$



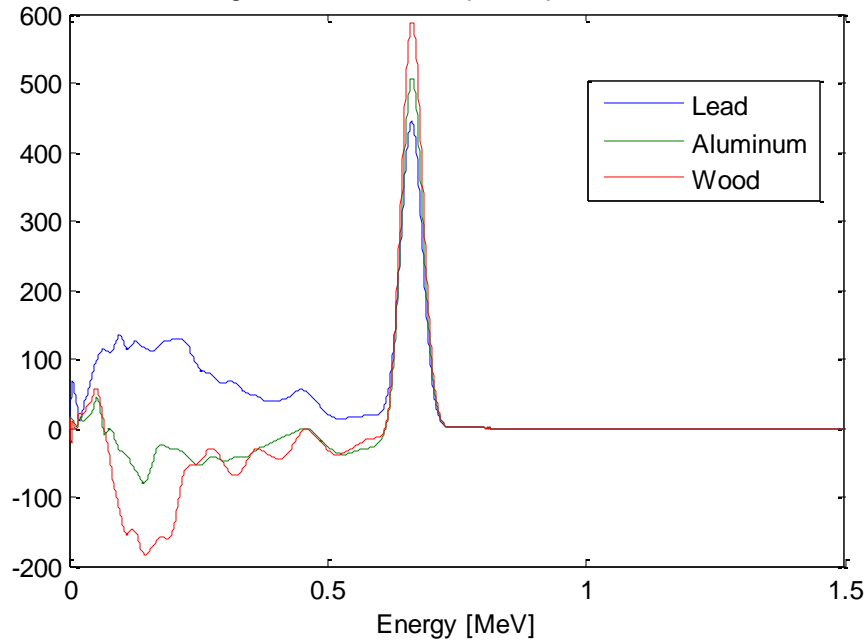
	Pb [cm]	Al [cm]	Wood [cm]
50%	0.53754	3.42235	10.72411
Standard	0.358364	2.281566	7.1493867
-50%	0.179182	1.140782	3.57470333



Second Finite Differences

$$\frac{\partial^2 \vec{f}_1}{\partial x_1^2} \approx \frac{\vec{f}_1(x_{1,p}, x_{2,s}, x_{3,s}) - 2\vec{f}_1(x_{1,s}, x_{2,s}, x_{3,s}) + \vec{f}_1(x_{1,m}, x_{2,s}, x_{3,s}))}{h_1^2}$$

Second order shielding derivatives Counts per h² per 20mCi Cs-137 at 1m, 2x4 NaI



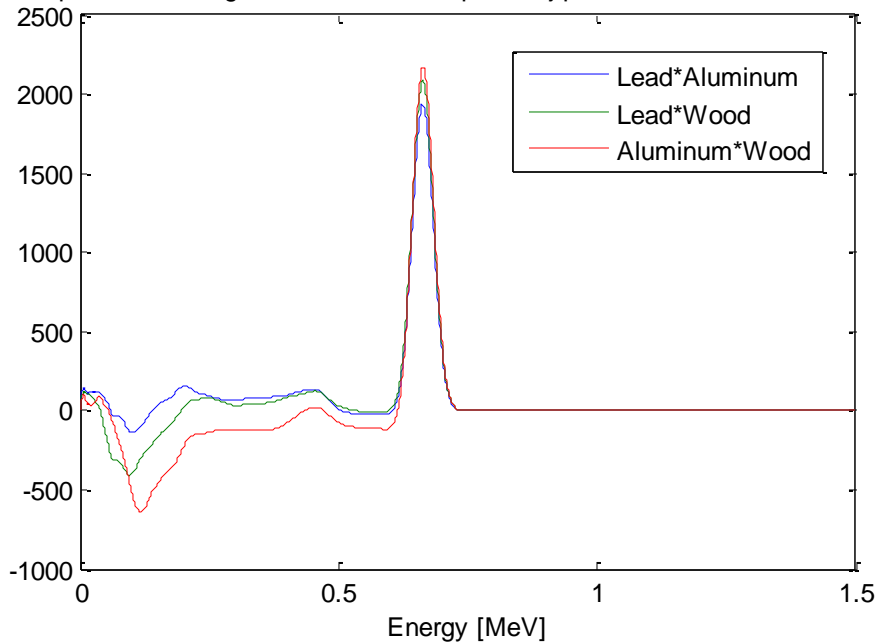
	Pb [cm]	Al [cm]	Wood [cm]
50%	0.53754	3.42235	10.72411
Standard	0.358364	2.281566	7.1493867
-50%	0.179182	1.140782	3.57470333

$$\begin{aligned} \vec{f}(\vec{x} + \Delta\vec{x}) = a & \left[\vec{f}_1(\vec{x}_0) + \frac{\partial \vec{f}_1}{\partial x_1} \Delta x_1 + \frac{\partial \vec{f}_1}{\partial x_2} \Delta x_2 + \frac{\partial \vec{f}_1}{\partial x_3} \Delta x_3 + \frac{1}{2} \frac{\partial^2 \vec{f}_1}{\partial x_1^2} \Delta x_1^2 + \frac{1}{2} \frac{\partial^2 \vec{f}_1}{\partial x_2^2} \Delta x_2^2 + \frac{1}{2} \frac{\partial^2 \vec{f}_1}{\partial x_3^2} \Delta x_3^2 \right. \\ & + \left(\frac{\partial^2 \vec{f}_1}{\partial x_1 \partial x_2} + \frac{\partial^2 \vec{f}_1}{\partial x_2 \partial x_1} \right) \Delta x_1 \Delta x_2 + \left(\frac{\partial^2 \vec{f}_1}{\partial x_1 \partial x_3} + \frac{\partial^2 \vec{f}_1}{\partial x_3 \partial x_1} \right) \Delta x_1 \Delta x_3 \\ & \left. + \left(\frac{\partial^2 \vec{f}_1}{\partial x_2 \partial x_3} + \frac{\partial^2 \vec{f}_1}{\partial x_3 \partial x_2} \right) \Delta x_2 \Delta x_3 \right] \end{aligned}$$

Mixed Partial Finite Differences

$$\frac{\partial^2 \vec{f}_1}{\partial x_1 \partial x_2} \approx \frac{\vec{f}_1(x_{1,p}, x_{2,p}, x_{3,s}) - \vec{f}_1(x_{1,p}, x_{2,m}, x_{3,s}) - \vec{f}_1(x_{1,m}, x_{2,p}, x_{3,s}) + \vec{f}_1(x_{1,m}, x_{2,m}, x_{3,s})}{4h_1 h_2}$$

Mixed partial shielding derivatives Counts per hi*hj per 20mCi Cs-137 at 1m, 2x4 Nal

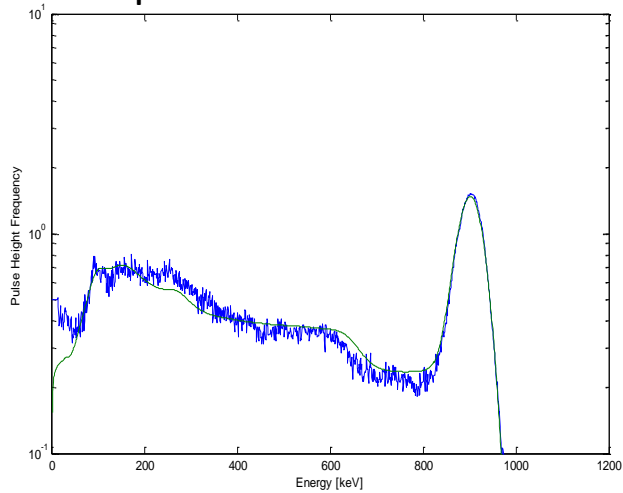


	Pb [cm]	Al [cm]	Wood [cm]
50%	0.53754	3.42235	10.72411
Standard	0.358364	2.281566	7.1493867
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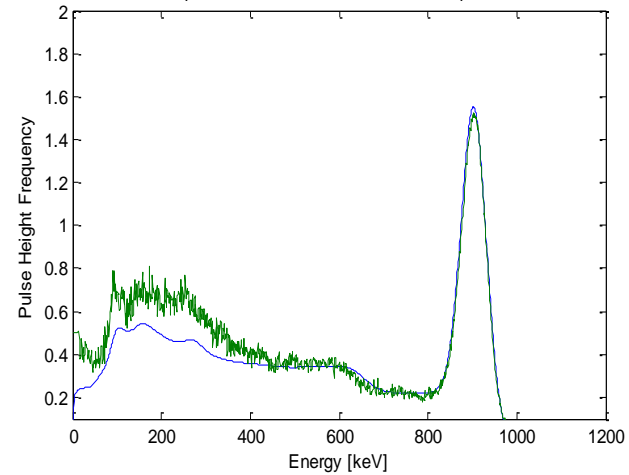
$$\vec{f}(\vec{x} + \Delta\vec{x}) = a \left[\vec{f}_1(\vec{x}_0) + \frac{\partial \vec{f}_1}{\partial x_1} \Delta x_1 + \frac{\partial \vec{f}_1}{\partial x_2} \Delta x_2 + \frac{\partial \vec{f}_1}{\partial x_3} \Delta x_3 + \frac{1}{2} \frac{\partial^2 \vec{f}_1}{\partial x_1^2} \Delta x_1^2 + \frac{1}{2} \frac{\partial^2 \vec{f}_1}{\partial x_2^2} \Delta x_2^2 + \frac{1}{2} \frac{\partial^2 \vec{f}_1}{\partial x_3^2} \Delta x_3^2 + \left(\frac{\partial^2 \vec{f}_1}{\partial x_1 \partial x_2} + \frac{\partial^2 \vec{f}_1}{\partial x_2 \partial x_1} \right) \Delta x_1 \Delta x_2 + \left(\frac{\partial^2 \vec{f}_1}{\partial x_1 \partial x_3} + \frac{\partial^2 \vec{f}_1}{\partial x_3 \partial x_1} \right) \Delta x_1 \Delta x_3 + \left(\frac{\partial^2 \vec{f}_1}{\partial x_2 \partial x_3} + \frac{\partial^2 \vec{f}_1}{\partial x_3 \partial x_2} \right) \Delta x_2 \Delta x_3 \right]$$

Example Results

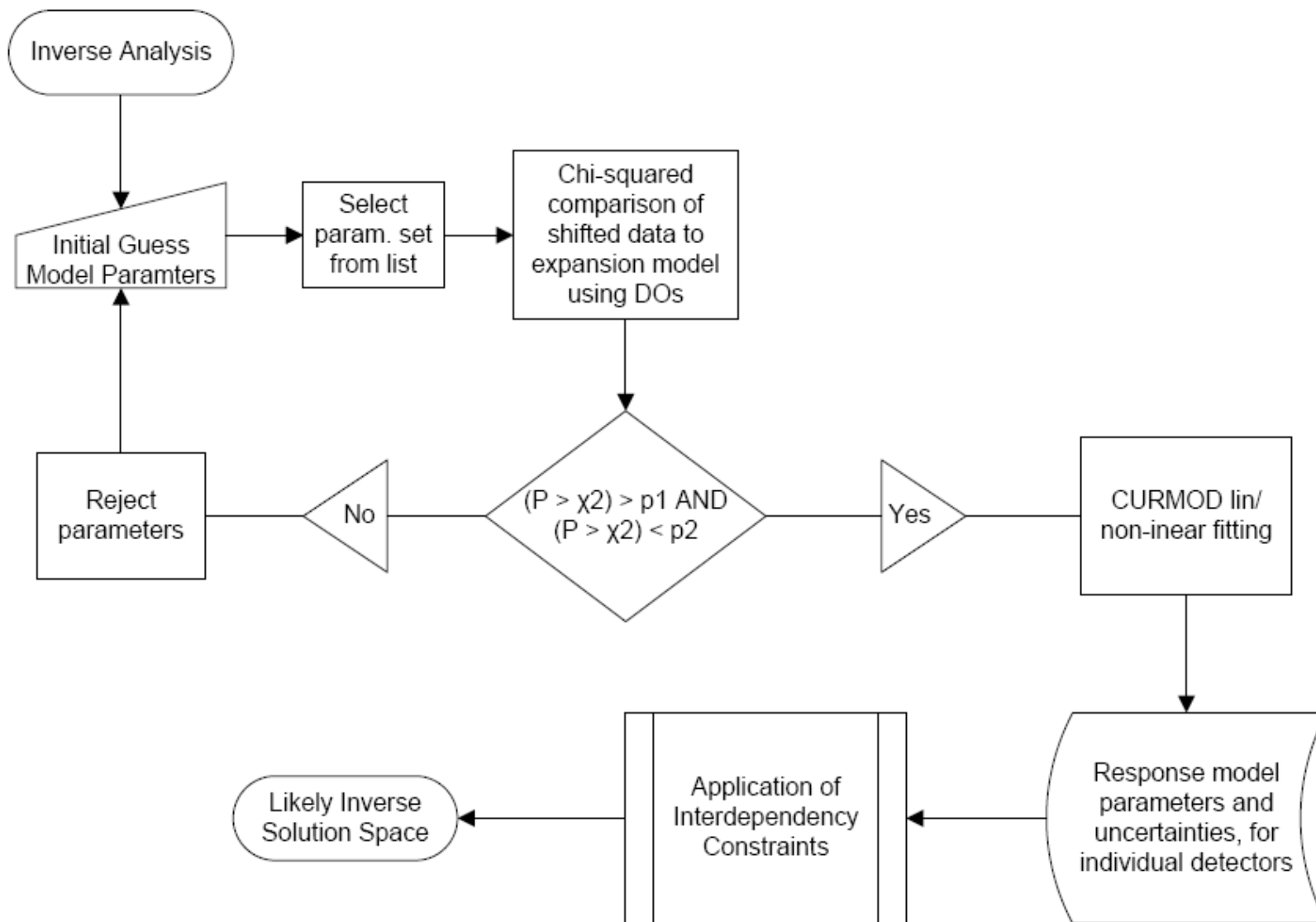
Experiment vs. model

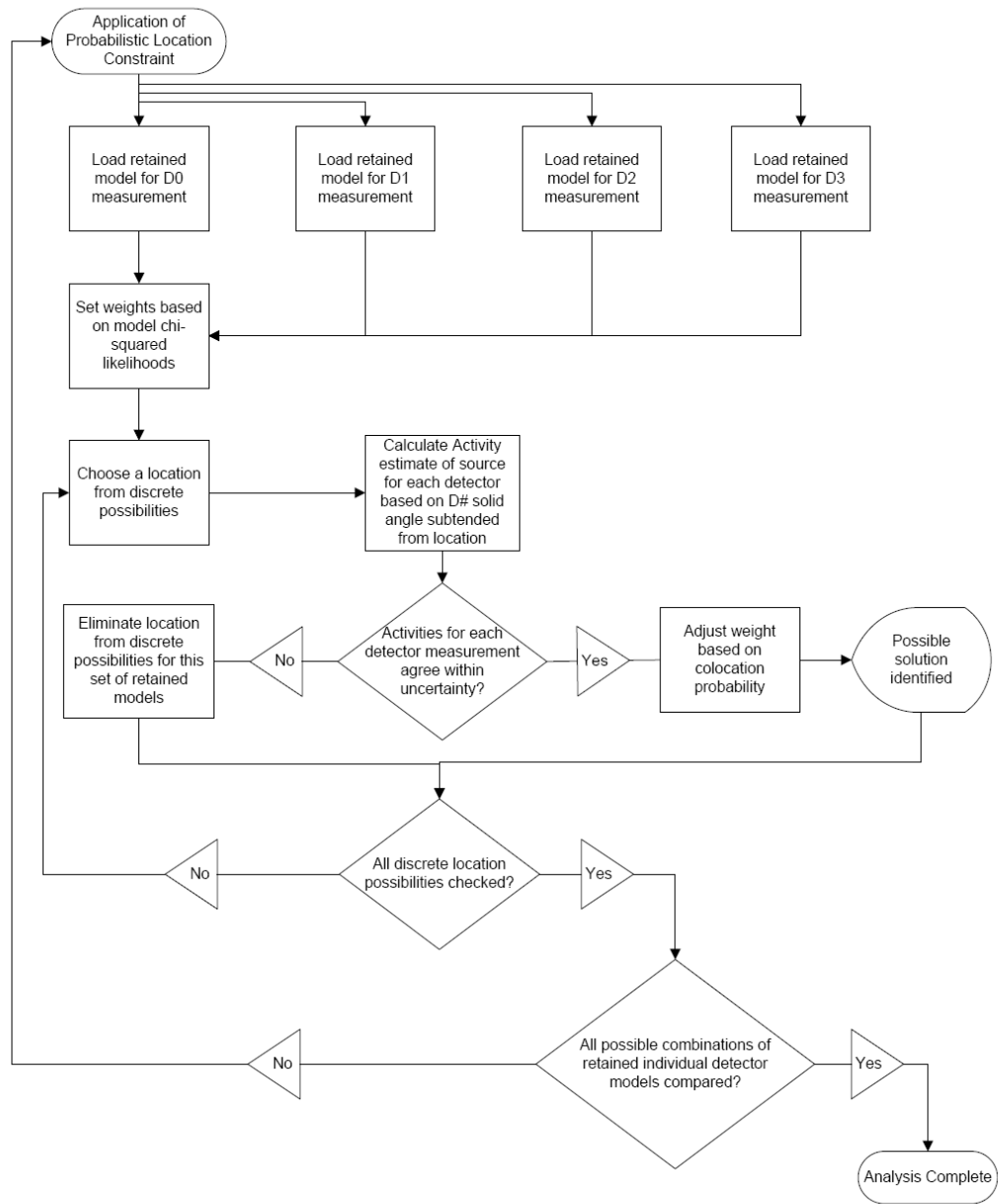


Comparison of 'sss' simulation to 'sss' experiment



	Pb thickness	Al thickness	Wood thickness	Activity	# of iteration
Actual	0.358 cm	2.282 cm	7.149 cm	4 μ Ci	N/A
Calculated 2nd	0.27 cm	1.83 cm	11.10 cm	3.21 μ Ci	56
Calculated 1st O	0.10 cm	0.99 cm	14.47 cm	2.74 μ Ci	148





Conclusion

- Passive gamma spec may have a decreasing role in cargo monitoring as it is costly and has limited impact for security, and is quite costly for the safety benefits it can produce.
- The MC LLS method has certain features that make it a viable platform for getting more out of a detection system.
 - Full spectrum analysis
 - Efficient linearization of L-M search algorithm
 - Highly customizable

Thank You!

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